

## Modelling and analysis of tool wear and surface roughness in hard turning of AISI D2 steel using response surface methodology

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### ABSTRACT

The present work deals with some machinability studies on tool wear and surface roughness, in finish hard turning of AISI D2 steel using PCBN, Mixed ceramic and coated carbide inserts. The machining experiments are conducted based on the response surface methodology (RSM). Combined effects of three cutting parameters viz., cutting speed, cutting time and tool hardness on the two performance outputs (i.e. VB and Ra), are explored employing the analysis of variance (ANOVA). The relationship(s) between input variables and the response parameters are determined using a quadratic regression model. The results show that the tool wear was influenced principally by the cutting time and in the second level by the cutting tool hardness. On the other hand, cutting time was the dominant factor affecting workpiece surface roughness followed by cutting speed. Finally, the multiple response optimizations of tool wear and surface roughness were carried out using the desirability function approach (DFA).

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### Nomenclature

$V_c$	cutting speed (m/min)	RSM	response surface methodology
$t$	cutting time (min)	df	degrees of freedom
$VB$	flank wear (mm)	HV	Vickers Hardness
$TH$	Cutting tool hardness (HV)	$b_j$	coefficients of linear terms
$HRC$	Rockwell Hardness	$b_{ii}$	quadratic terms
$R_a$	arithmetic mean roughness ( $\mu\text{m}$ )	$b_{ij}$	cross-product terms
$R^2$	determination coefficient		

### 1. Introduction

CBN, mixed ceramic and coated carbide tools are widely used in the manufacturing industry for cutting various hard materials such as high-speed tool steels, die steels, bearing steels, case-hardened steels, white and grey cast irons. In many applications, cutting of these hardened ferrous materials are produced mainly by a sequential series of processes, including costly and time consuming grinding and polishing

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operations. To meet these challenges, hard turning has emerged as an effective single step metal cutting process to replace grinding operation and give substantial savings in both cost and productivity rates (Lin et al., 2008). Hard turning process differs from conventional turning because of the workpiece hardness i.e., work-piece hardness range of 40-62 HRC (Özel et al., 2007). Hard turning offers a number of potential advantages over traditional grinding process, including shorter setup time, greater process flexibility, lower power consumption, fewer process steps and usually there is no need of coolant. Hard turning, if applied to fabricate complex parts, could reduce manufacturing costs up to 30 times (Huang et al., 2007).

Many studies have been conducted to investigate the performance of CBN, mixed ceramic and coated carbide tool in the cutting of various hardened materials. Bensouilah et al., (2016) applied taguchi based method to determine the effect of cutting parameters on cutting force and surface roughness components in hard turning of AISI D3 cold work tool steel using coated and uncoated CC650 ceramic inserts. The analysis of variance (ANOVA), the signal-to-noise ratio and response surface methodology (RSM) techniques were adopted. It was observed that the surface quality obtained with the coated ceramic insert was 1.6 times better than the one obtained with uncoated CC650 ceramic insert. However, the uncoated ceramic insert was useful in reducing the machining force.

Asiltürk and Akkas (2011) used taguchi experimental design to obtain optimum cutting parameters in minimizing surface roughness while turning hardened AISI 4140 (51 HRC) with coated carbide tools. Experiments were conducted using the L9 orthogonal array in a CNC turning machine. They also investigated the effects of cutting parameters on surface roughness by applying statistical methods of signal to noise ratio (SNR) and ANOVA. It was reported that the feed rate has the most significant effect on Ra and Rz. Davim and Figueira (2007) performed an experimental and statistical investigation of the machinability of AISI D2 tool steel. Hard turning operation was performed on AISI D2 steel having hardness 60 HRC, the tests were conducted by using cutting speed, feed rate and cutting time as main parameters and analysis was done based on the responses. The influence of cutting parameters under flank wear, surface roughness and cutting forces on machinability evaluation in turning with wiper and traditional ceramic tools using ANOVA was presented. Cutting time and cutting velocity were found to be the main parameters that affected the flank tool wear of ceramic cutting tools. However, feed rate was the most influential parameter affecting surface roughness. It was also reported that wiper ceramic tools performed better than traditional ceramic tools.

Suresh et al., (2012) investigated the influences of machining parameters on surface roughness, tool wear, machining forces and cutting forces during machining of AISI 4340 steel with coated carbide tools using taguchi technique. The analysis of the result revealed that higher values of feed rates are necessary to minimize the specific cutting force. It was observed that the machining power and cutting tool wear increases almost linearly with increase in cutting speed and feed rate. Furthermore, it was reported that the combination of high cutting speed and low feed rate is important for minimizing the surface roughness. Azizi et al., (2012) investigated the influences of cutting speed, feed rate, depth of cut and workpiece hardness on surface roughness and cutting force during machining of AISI 52100 steel with coated mixed ceramic tools. Taguchi L27 orthogonal array was used for planning the experiments. Analysis of variance (ANOVA) was used to check the validity of linear regression model and to determine the significant parameters affecting the surface roughness and cutting forces. It was reported that the significant parameters in reducing surface roughness were feed rate, workpiece hardness and cutting speed, whereas, depth of cut, workpiece hardness and feed rate were statistically significant on the cutting force components.

Elbah et al., (2013) have presented a comparative investigation between the roughness criteria of wiper and uncoated ceramic inserts in hard turning of AISI 4140 steel. To check the validity of quadratic regression model and to determine the significant parameter affecting the surface roughness, RSM and ANNOVA were used. They observed that the surface quality obtained with the wiper ceramic insert was

2.5 times better than the uncoated ceramic insert. Moreover, it was also reported that the feed rate and depth of cut were the most significant factors in reducing the surface roughness. Aouici et al. (2014) used a  $3^3$  full factorial design, 27 experiments were carried out to determine the effects of feed, cutting speed, and depth of cut on surface roughness, power, and specific cutting force in hard turning of AISI D3 hardened steel using ceramic cutting tool. It was observed that the feed rate is the most influencing factor on surface roughness. Cutting force was affected mostly by feed rate followed by depth of cut. They recommended machining with lower depth of cut and higher cutting speed and recommended limiting the range of feed rate (0.12-0.13 mm/rev) to ensure better surface roughness and minimum cutting forces.

Özel et al., (2005) used a four-factor, two-level factorial design (24) with 16 replications to determine the effects of cutting tool edge geometry, feed rate workpiece hardness and cutting speed on resultant forces and surface roughness in finish hard turning of AISI H13 steel using CBN tools. It was reported that the effect of cutting edge geometry was very significant on the surface roughness. Honed edge geometry and lower workpiece surface hardness resulted in better surface roughness. Also, it was reported that workpiece hardness, cutting edge geometry and cutting speed significantly influenced the force component. Aouici et al., (2012) studied the effects of cutting speed; feed rate, depth of cut and work-piece hardness on surface roughness and force components in hard turning of AISI H11 steel using CBN tools. Mathematical models and analysis of results were performed using RSM. The results demonstrated that feed rate and workpiece hardness were the significant parameters affecting surface roughness, whereas depth of cut and work-piece hardness were principal parameters influencing cutting force components. Bouacha et al. (2010) applied response surface methodology (RSM) to investigate the effect of cutting parameters on cutting force and surface roughness components in hard turning of AISI 52100 with CBN tool. The results showed that feed rate and cutting speed parameters mainly influenced surface roughness, while depth of cut exhibited maximum influence on the cutting forces as compared to feed rate and cutting speed. Sahin (2009) compared the tool life of coated CBN, uncoated and coated ceramic inserts in hard turning of AISI 52100 bearing steel using the Taguchi method. The effects of cutting speed, tool hardness and feed rate on tool life were determined by using orthogonal array, signal to noise ratio (SNR) and ANOVA. It was reported that the effects of cutting speed followed by tool hardness and feed rate on tool life were 41.63%, 32.68% and 25.22%, respectively.

Several researchers have made attempts to optimize and understand the effect of various machining parameters using different techniques for the control of the turning process. Experiments on turning of various grades of steels were conducted using different kinds of cutting tools to identify different factors affecting surface roughness, tool wear, cutting force and power consumption (Chinchanikar & Choudhury, 2013; Gaitonde et al., 2009; Saravanan et al., 2015; Tamang & Chandrasekaran, 2015). In the pre-cited general framework, most of the machining studies have been focused on hard and hardened steels using ceramic or CBN cutting tools. However, relatively few works related to machining steels or hardened steels based on the tool wear or surface roughness prediction models have been reported by the response surface methodology. The main objective of the present study is to analyze the effects of machining operation parameters such as cutting speed, cutting time and cutting tool hardness on different aspects like tool wear and surface roughness. The novelty of the present work lies in the comparison between the performance of mixed ceramic, CBN and coated carbide inserts when machining AISI D2 cold work steel using combination of cutting speed, cutting time and tool hardness as input parameters. Particularly the effect of cutting parameters on surface roughness and tool wear of the inserts is highlighted by applying RSM methodology.

## **2. Experimental procedure**

### *2.1. Workpiece and tool materials*

Turning experiments were performed in dry conditions on a heavy duty lathe (HMT make) with 5.2 kW spindle power. The workpiece material was AISI D2, cold work steel, which is popularly used in

stamping and punching operations. The composition of the as received material used in this study is listed in Table 1. The workpiece was thorough-hardened steel followed by a tempering process to attain a hardness value of 45.1 HRC (442 HV). Removable type cutting inserts with four squared working edges were used in the study. The cutting tools used are commercially available and are manufactured by Sandvik coromant. The chemical composition and physical properties of cutting inserts are summarized in Table 1.

**Table 1**  
Workpiece material and cutting tool descriptions

Material	Name/Description	Composition	Hardness
Work-piece	AISI D2	Chem. Comp :C (1.70),Si (0.30), Mn (0.30), Cr (12.00 ), W(0.50),V(0.10),Mo (0.60), Fe (balance)	45.1 HRC (442 HV)
Cutting tools	Mixed Alumina	70%Al <sub>2</sub> O <sub>3</sub> +30% TiC	2200 HV
	PCBN	CBN +TiN binder +TiN coating	2950 HV
	Coated Carbide	Multilayer TiC/TiCN/Al <sub>2</sub> O <sub>3</sub> coated by TiN over a carbide tool	1635 HV

The cutting inserts were clamped to a right-hand tool holder with ISO designation PCLNR 25 25 M 12 having  $-6^\circ$  rake angle,  $-6^\circ$  clearance angle, and  $95^\circ$  approach angle. Instantaneous roughness criteria measurements (arithmetic mean roughness, Ra), for each cutting condition, are obtained by means of a contact stylus profilometer - Hommel Etamic, Jenoptik, Germany, (Model W5) with traverse length of 3.20 mm and cut-off width of 0.8 mm with a stylus tip radius of 2  $\mu$ m. The flank tool wear was evaluated by Leica DM 6000 advanced microscope and having image characterized, using Leica image analysis software.

## 2.2. Experimental design

### 2.2.1. Response surface methodology

The objective of response surface methodology (RSM) is to determine a relationship between independent input process parameters with the studied responses (Gaitonde et al., 2010). This procedure includes following six steps (Aouici et al., 2012). These are, (1) definition of independent input variables and the desired output responses, (2) adoption of an experimental design plan, (3) performing regression analysis with the quadratic model of RSM, (4) calculate analysis of variance (ANOVA) for the independent input variables in order to find significant parameters that affect the responses, (5) determination of the situation of the quadratic model of Response Surface Methodology and decide whether the model of RSM needs screening variables or not and finally, (6) optimization, conduction of confirmation experiments and verifying the predicted performance characteristics. In the current study, the relationship between the input, called the cutting conditions, cutting speed ( $V_c$ ), cutting time ( $t$ ), tool hardness (TH) and the output  $Y$ , defined as the desired machinability (tool wear, surface roughness,) is given as

$$Y = \emptyset ( V_c, t, TH ), \quad (1)$$

where  $\emptyset$  is the response function. The approximation of  $Y$  is proposed by using a quadratic mathematical model, which is suitable for studying the interaction effects of process parameters on machinability characteristics. In the present context, the RSM based second order mathematical model is given by:

$$Y = b_0 + \sum_{i=1}^k b_i X_i + \sum_{ij}^k b_{ij} X_i X_j + \sum_{i=1}^k b_{ii} X_i^2, \quad (2)$$

where  $b_0$  is the free term of the regression equation, the coefficients,  $b_1, b_2, b_3, \dots, b_k$  are the linear terms and  $b_{11}, b_{22}, \dots, b_{kk}$  are quadratic terms while  $b_{12}, b_{13}, b_{k-1}$  are the interacting terms.  $X_i$  represents input parameters (Vc, t, and TH). The output, tool wear (VB) and surface roughness (Ra) are also called response factors.

Face central composite design (FCCD) test matrix with an alpha value of 1 was used for planning of tool wear and surface roughness experiments. In the present work, 20 experiments were performed on the work material to develop tool wear and surface roughness models. The experimental plan is developed to assess the influence of cutting speed (Vc), cutting time (t) and tool hardness (TH) on the surface roughness (Ra) and tool wear (VB) parameter. The levels of the three factors on machining parameters are reported in Table 2 and the experimental design consists of 20 runs as outlined in Table 3.

**Table 2**

Assignment of the factor levels

S. No	Parameters	Units	Low level	High level
1	Cutting speed	m/min	-1	+1
2	Cutting time	mins.	-1	+1
3	Tool hardness (TH)	HV	-1	+1

**Table 3**

Experimental results for tool wear and surface roughness parameters

Run.no	Machining parameters			Response factors	
	Cutting speed Vc (m/min)	Cutting time t (mins.)	Tool Hardness TH(HV)	Tool wear VB( $\mu$ m)	Surface roughness Ra( $\mu$ m)
1	150	4	2950	151.22	0.85
2	190	4	2200	160.61	0.94
3	190	2	1635	127.39	0.71
4	150	4	2200	149.05	0.81
5	150	4	2200	136.45	0.67
6	110	2	1635	107.68	0.51
7	150	4	2200	138.30	0.73
8	150	4	2200	132.54	0.71
9	150	4	1635	224.82	1.02
10	150	4	2200	145.56	0.77
11	190	6	2950	220.74	0.99
12	110	2	2950	68.39	0.32
13	150	2	2200	103.43	0.50
14	150	4	2200	151.11	0.87
15	150	6	2200	173.14	1.20
16	110	6	2950	139.10	0.53
17	110	4	2200	122.56	0.38
18	190	6	1635	290.00	1.88
19	110	6	1635	207.57	1.17
20	190	2	2950	94.93	0.67

### 3. Results and discussion

Table 3 shows all the values of the response factors, tool wear and surface roughness components. The surface roughness (Ra) was obtained in the range of (0.32–1.88)  $\mu$ m and tool wear was obtained in the range (68.39–290)  $\mu$ m, respectively.

#### 3.1. Statistical analysis

A variance analysis of the tool wear (VB) and the surface roughness (Ra) components was made with the objective of analyzing the influence of cutting speed (Vc), cutting time(t), and cutting tool hardness (TH) on the results. Tables 4 and Table 5 show these results of ANOVA, respectively, for tool wear (VB) and surface roughness (Ra). ANOVA was performed using Design Expert 10 statistical software. The

analysis was out for 5% significance level, i.e., for 95% confidence level. Table 4 presents the ANOVA results for tool wear. The Model F-value of 30.47 implies the model is significant. Values of "Prob > F" less than 0.0500 indicate model terms are significant. The "Lack of Fit F-value" of 5.27 implies there is a 4.60% chance that a "Lack of Fit F-value" could occur due to noise. "Adeq Precision" measures the signal to noise ratio. A ratio greater than 4 is desirable. The ratio of 22.624 indicates an adequate signal. It is, therefore, concluded that this model is significant and can be used to navigate the design space. The sum of squares, the mean square, the F value as well as the residual is shown in the ANOVA table. Cutting speed (Vc), cutting time (t), cutting tool hardness (TH); interaction effect of cutting speed and cutting time (Vc × t) and the square of cutting tool hardness (TH)<sup>2</sup> have significant effect on the tool wear. But the effect of cutting time (57%) and tool hardness (23%) are the most significant factors associated with tool wear. The analysis of influence on surface roughness is summed up in Table 5. The value of "P-value" for model is less than 0.05 which indicates that the model is significant, which is desirable as it indicates that model terms have a significant effect on the output response. For "adeq precision" the signal to noise ratio is 22.028 (>4) which indicates an adequate signal and therefore the model is significant and can be used to navigate the design space. It is, therefore, concluded that this model. Cutting time (t) cutting speed (Vc) and tool hardness (TH), interaction of cutting speed and cutting time (Vc × t), interaction of cutting time and tool hardness (t × TH), product of cutting time (t<sup>2</sup>) and product of tool hardness (TH<sup>2</sup>) are found to be significant factors and contributed more for the surface roughness response. The cutting time (45%) followed by the cutting speed (22.8%) and tool hardness (18.4%) had the most effect on surface roughness.

**Table 4**

ANOVA results for tool wear (VB)

Source	Sum of Squares	df	Mean Square	F Value	p-value Prob > F		
Model	47999.47	9	5333.27	30.47	< 0.0001	significant	
Vc	6020.22	1	6020.22	34.39	0.0002		
t	28417.23	1	28417.23	162.33	< 0.0001		
TH	11485.02	1	11485.02	65.61	< 0.0001		
Vc × t	1734.81	1	1734.81	9.91	0.0104		
Vc × TH	7.35	1	7.35	0.042	0.8418		
t × TH	461.82	1	461.82	2.64	0.1354		
Vc <sup>2</sup>	288.84	1	288.84	1.65	0.2279		
t <sup>2</sup>	504.94	1	504.94	2.88	0.1203		
TH <sup>2</sup>	4414.24	1	4414.24	25.22	0.0005		
Residual	1750.62	10	175.06				
Lack of Fit	1471.47	5	294.29	5.27	0.0460		not significant
Pure Error	279.15	5	55.83				
Cor Total	49750.09	19					

Std. Dev. = 13.23 Mean = 152.23 C.V. = 8.69 % R-Squared = 0.9648 Adj R-Squared = 0.933 Adeq precision = 22.624

**Table 5**

ANOVA results for surface roughness (Ra)

Source	Sum of Squares	df	Mean Square	F Value	p-value Prob > F		
Model	2.19	9	0.24	28.33	< 0.0001	significant	
Vc	0.52	1	0.52	60.80	< 0.0001		
t	1.04	1	1.04	120.80	< 0.0001		
TH	0.42	1	0.42	48.93	< 0.0001		
Vc × t	0.045	1	0.045	5.26	0.0448		
Vc × TH	1.667E-003	1	1.667E-003	0.19	0.6689		
t × TH	0.21	1	0.21	24.62	0.0006		
Vc <sup>2</sup>	0.047	1	0.047	5.43	0.0421		
t <sup>2</sup>	0.011	1	0.011	1.32	0.2766		
TH <sup>2</sup>	0.081	1	0.081	9.40	0.0119		
Residual	0.086	10	8.590E-003				
Lack of Fit	0.060	5	0.012	2.34	0.1864		not significant
Pure Error	0.026	5	5.147E-003				
Cor Total	2.28	19					

Std. Dev. = 0.093 Mean = 0.82 C.V. = 11.37 % R-Squared = 0.9623 Adj R-Squared = 0.9283 Adeq precision = 22.028

### 3.2. Regression equations

The relationship between the factors and the performance measures were modelled by quadratic regression. The regression equations obtained were as follows. The tool wear (VB) model is given below in Eq. (3). Its coefficient of determination ( $R^2$ ) is 96.48%

Final equation in terms of actual factors:

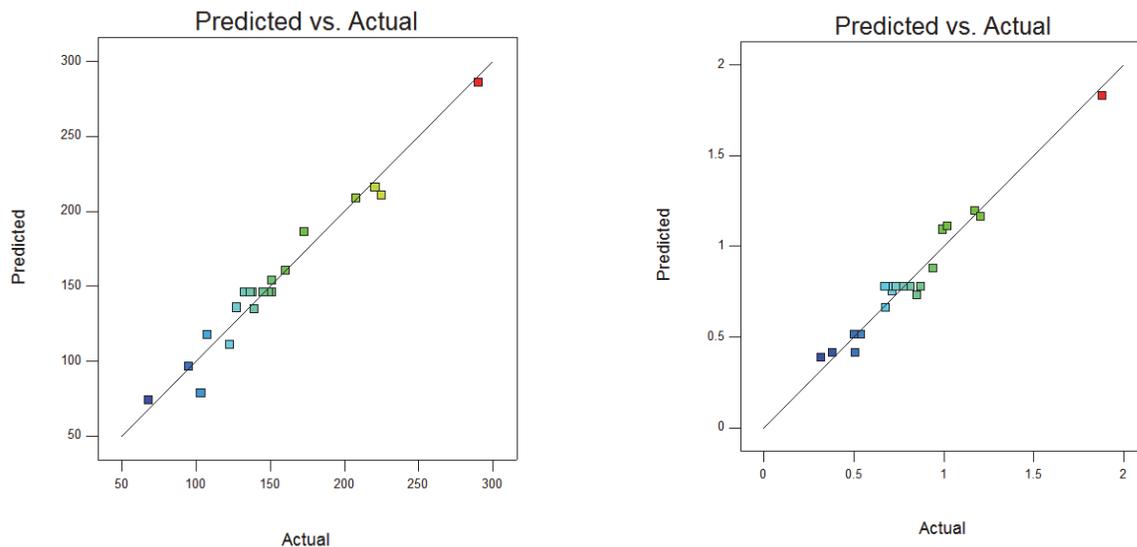
$$\begin{aligned} \text{Tool Wear (VB)} = & 411.391 + 1.72352 \times Vc + 39.0394 \times t - 0.460125 \times TH + 0.184073 \times Vc \times \\ & t + 3.63656e-005 \times Vc \times TH - 0.00576643 \times t \times TH - 0.00640531 \times Vc^2 - 3.38763 \times t^2 + \\ & 9.48049e-005 \times TH^2 \end{aligned} \quad (3)$$

The surface roughness model  $R_a$  is given in Eq. (4). Its coefficient of determination ( $R^2$ ) is 96.23%

Final equation in terms of actual factors:

$$\begin{aligned} \text{Surface roughness} = & -0.245263 + 0.0276161 \times Vc + 0.164338 \times t - 0.0015745 \times TH + \\ & 0.000939063 \times Vc \times t - 5.47811e-007 \times Vc \times TH - 0.00012341 \times t \times TH - 8.13636e-005 \times t^2 \\ & + 0.0160795 \times t^2 + 4.05398e-007 \times TH^2 \end{aligned} \quad (4)$$

The predicted values of response factors illustrating tool wear (VB) and surface roughness ( $R_a$ ), are obtained from regression Eqs. (3-4) and the experimental values corresponding to different combinations of machining parameters are reported in Table 4. The predicted values are compared with the corresponding experimental values. This is depicted in Fig. 1 and Fig. 2.



**Fig. 1.** Comparison between measured and predicted values for tool wear **Fig. 2.** Comparison between measured and predicted values for surface roughness

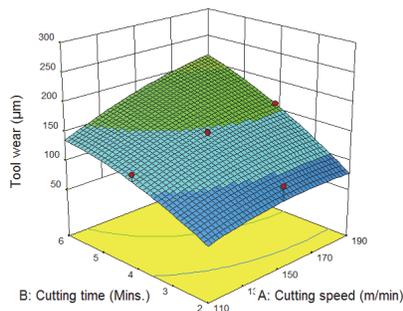
### 3.3 Effect of machining parameters on surface response parameters

#### 3.3.1 Tool Wear

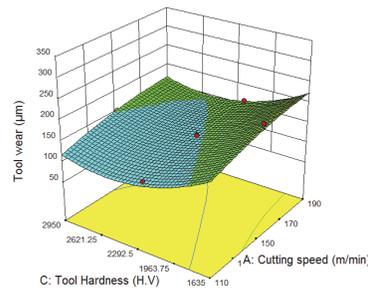
The analysis of ANOVA Table 4 indicates that the cutting time ( $t$ ) followed by cutting tool hardness ( $TH$ ) and cutting speed ( $Vc$ ) had the highest influence on tool wear. Interaction of cutting speed and cutting time ( $Vc \times t$ ) and the product of tool hardness ( $TH^2$ ) maintained negligible effect or are less

significant on tool wear. Interaction plots, in Figs (3-5), illustrate the evolution of the tool wear (flank wear) according to the cutting speed ( $V_c$ ), cutting time ( $t$ ) and tool hardness (TH) parameters. Fig. 3 shows the estimated response surface for the tool wear in relation to the cutting time and cutting speed. According to the figure, the increasing effects of cutting speed and cutting time increases tool wear. It was also observed from the figure that cutting time exhibits the maximum influence on tool wear, as was also reported by (Berkani et al., 2015). This is due the fact that with the increase in cutting speed (110-190 m/min), the rubbing action between the cutting tool and the workpiece material is faster and more heat is produced even though less contact time exists. This increased temperature at contact zone with increased speed is significantly high, which even causes the cutting material to exceed its limit of thermal stability. This generation of heat, at the flank face of the tool, softens the cutting edge and more wear occurs (Suresh et al., 2012). The maximum value of tool flank wear was found with high levels of cutting time and cutting speed.

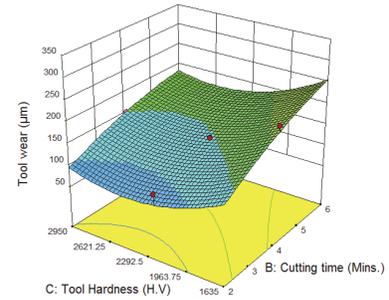
From the interaction plots Fig. 4 and Fig. 5, it can be observed that, the tool wear has a tendency to reduce with increase in tool hardness up to a certain point with all cutting speeds used. Conversely, the figures also indicate that the increase of tool hardness from 2200 HV to 2950 HV leads to the increase of tool wear with increasing time and cutting speed. From the above discussion and the study of Figs. (4-5), it is obvious that the characteristic wear of tool is caused by the fact that, the speed and time are the influential factor on wear and it is more likely that wear is the consequence of the speed and time of cut. From the above discussions, it is clear that a combination of middle values of tool hardness, low cutting speed, and minimum cutting time is favorable in reducing tool wear.



**Fig. 3.** Effect of cutting speed and cutting time on tool wear



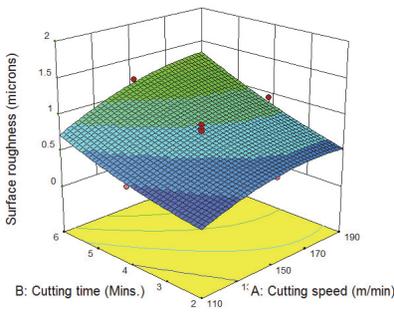
**Fig. 4.** Effect of cutting speed and tool hardness on tool wear



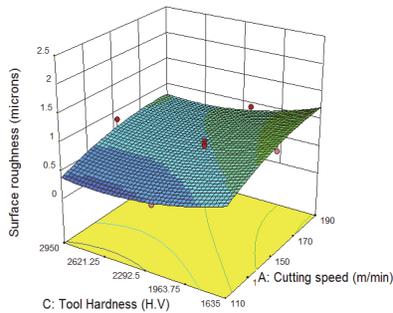
**Fig. 5.** Effect of cutting time and tool hardness on tool wear

### 3.3.2 Surface Roughness

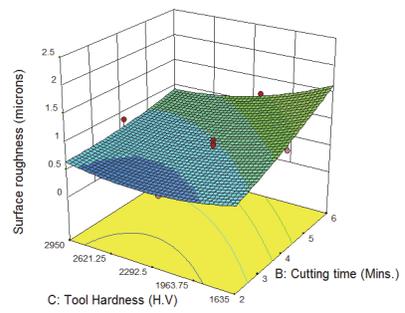
The estimated response surface for the surface roughness in relation to the cutting parameters cutting speed, cutting time and tool hardness is presented in Figs 5-8. From Fig 5, it can be observed that the cutting time ( $t$ ) and cutting speed ( $V_c$ ) had a significant influence on machined surface roughness ( $R_a$ ). It is observed that the surface roughness increases with the increase in the machining time ( $t$ ) due to the wear development, as reported by Bensouliah et al. (2016). Further, increasing the cutting speed causes a drastic increase in surface roughness because the cutting tool nose wear increases, causing more surface roughness. Maximum surface roughness was obtained at the combination of highest cutting speed ( $V_c$ ) and maximum cutting time ( $t$ ). Figs (6-7) explain the main effects of cutting speed ( $V_c$ ), cutting time ( $t$ ) and tool hardness (TH) on the surface roughness of the work-piece. The tool hardness effect on surface roughness has a medium statistical importance. Moreover, it can be deduced from the figures that the interaction of higher values of cutting speed ( $V_c$ ) and cutting time ( $t$ ) with higher values of tool hardness (TH) has tendency to reduce the surface roughness values. This might be due to retention of cutting edge at higher temperature, caused due to maximum cutting speed ( $V_c$ ) and maximum contact time ( $t$ ). The best surface roughness was achieved at the middle level of tool hardness (TH) with low cutting speed ( $V_c$ ) and minimum time ( $t$ ).



**Fig. 6.** Effect of cutting speed and cutting time on surface roughness



**Fig.7.** Effect of cutting speed and tool hardness on surface roughness



**Fig. 8.** Effect of cutting time and tool hardness on surface roughness

**3.4 Optimization of cutting conditions**

Desirability function is not a direct optimization method (Berkani et al., 2015). It has been used to optimize multiple response factors (VB and Ra). Desirability function is a decision support tool used to identify process parameters that results in near-optimal settings for process responses. During the optimization process, the aim is to find the optimum values of machining parameters in order to produce the lowest tool wear and minimize surface roughness (VB and Ra). Table 6 summarizes the goals and parameter ranges for the optimization process. The RSM optimization results for VB and Ra are defined in Table 7 in order of their decreasing desirability levels. The optimized tool wear (VB) and surface roughness (Ra) results are (54.868-74.043)  $\mu\text{m}$  and (0.234-0.531)  $\mu\text{m}$ , respectively.

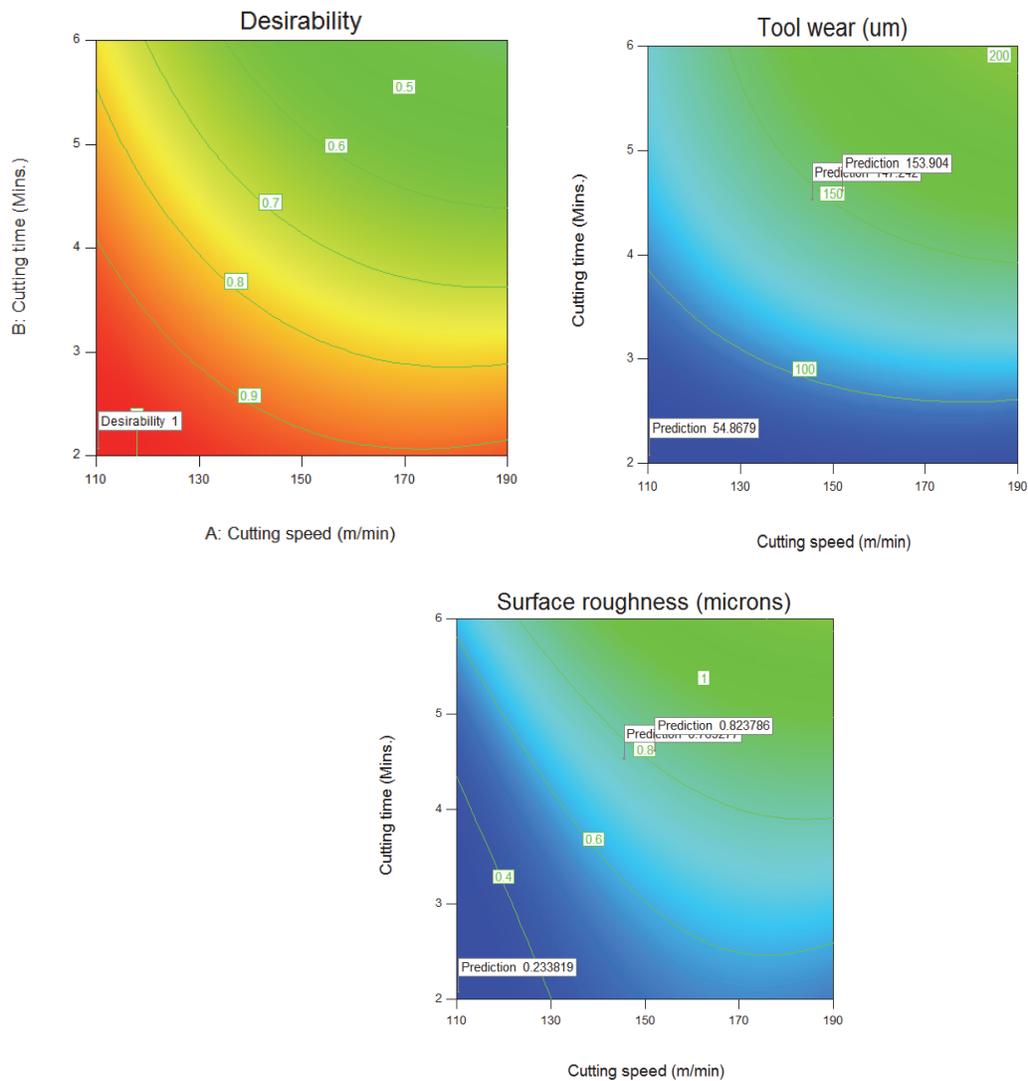
Fig. 9 shows two dimensional contour plots that explain the optimization results in terms of composite desirability. The figure clearly explains that the increasing cutting speed and cutting time decreases the composite desirability level.

**Table 6**  
Goals and parameter ranges for optimization of cutting conditions

Name	Goal	Lower Limit	Upper Limit	Lower Weight	Upper Weight	Importance
Cutting speed	is in range	110	190	1	1	3
Cutting time	is in range	2	6	1	1	3
Tool Hardness(TH)	is in range	1200	2950	1	1	3
Tool wear	minimize	68.39	290	1	1	5
Surface roughness	minimize	0.32	1.88	1	1	5

**Table 7**  
Response optimizations for tool wear and surface roughness parameters

Number	Cutting speed	Cutting time	Tool Hardness(TH)	Tool wear	Surface roughness	Desirability
1	110.439	2.072	2395.336	54.868	0.234	1.000
2	117.144	2.087	2183.856	67.453	0.308	1.000
3	112.079	2.222	2445.409	60.336	0.260	1.000
4	111.715	2.121	2320.841	58.993	0.248	1.000
5	112.531	2.069	2515.391	56.088	0.267	1.000
6	152.169	2.000	2350.732	74.043	0.515	0.924
7	190.000	2.000	2420.366	72.627	0.529	0.922
8	190.000	2.000	2403.479	72.752	0.529	0.922
9	189.999	2.010	2441.076	73.029	0.531	0.920



**Fig. 9.** Composite desirability for tool wear and surface roughness

#### 4. Conclusions

This paper presented an investigation of cutting parameters effect on tool wear and surface roughness in machining of AISI D2 steel. Mathematical models were developed to define a relationship between input parameters (cutting speed, cutting time and tool hardness) and output variables using Response surface methodology (RSM). Analysis of variance (ANOVA) was used to check the adequacy of the model and its respective variables. Combined effects of machining parameters on tool wear and surface roughness were evaluated through 3D surface graphs. Finally, the multiple response optimizations of tool wear (VB) and surface roughness (Ra) were carried out using the desirability function approach (DFA). Following conclusions can be drawn from this study:

1. The analysis of machining parameters, using RSM approach, allows the investigation of the influence of each factor on the response outputs, such as tool wear and surface roughness.
2. ANOVA table for tool wear has shown that the main effects of cutting time, tool hardness, cutting speed, the product of tool hardness and the interaction effect of cutting speed and cutting time, all had significant effect on tool wear. Moreover, the cutting time had the most effect on tool wear (57%) followed by cutting tool hardness (23%).

3. ANOVA table for surface roughness has shown that the main effects of cutting time, cutting speed, tool hardness, the product of cutting speed, the product of tool hardness, the interaction effect of cutting speed and cutting time ( $V_c \times t$ ) and the interaction of cutting time and tool hardness ( $t \times TH$ ) had significant effects on surface roughness. Moreover, the cutting time (45%), the cutting speed (22.8%) had the most effect on surface roughness.

4. Based on multi-response optimization process, the optimum cutting variables for minimum tool wear with maximum surface finish were cutting speed of 110.439 m/min, cutting time of 2.072 mins and tool hardness of 2395.336 respectively.

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